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(\$4) Title: PROCESS FOR PRODUCING POLYFLUOROACYL COMPOSITIONS				

(57) Abstract

A process is disclosed for preparing polyhaloacyl fluorides such as trifluoroacetyl fluoride and difluoroacetyl fluoride by oxidizing 1-chloro-1,2,2,2-trifluoroethanes and 1,1-dichloro-2,2-difluoroethane, respectively with oxygen.

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TITLE

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PROCESS FOR PRODUCING POLYFLUOROACYL COMPOSITIONS

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Field of the Invention

The instant invention relates to an oxidative process for producing polyfluoroacyl fluorides, chlorides and free acids thereof. More particularly, the instant invention relates to a process which comprises oxidizing at least one polyfluoroalkyl-substituted dichloro-or chlorofluoro-methane. One aspect of the invention relates to oxidizing 1-chloro-1,2,2,2-tetrafluoroethane, CHClFCF3 (HCFC-124) to trifluoroacetyl fluoride, CF3COF (TFAF), as the predominant acetyl product, which may be accompanied by lesser amounts of one or more of trifluoroacetyl chloride (TFAC) and trifluoroacetic acid (TFAA). Another aspect of the invention relates to oxidizing 1,1-dichloro-2,2-difluoroethane, CHCl2CHF2 (HCFC-132a), to form a product stream comprising difluoroacetyl fluoride. CHF2COF (DFAF), difluoroacetyl chloride (DFAC), and the free acid, CHF2COOH (DFAA).

The polyfluoroacyl fluorides and chlorides are broadly useful as acylating agents for producing agricultural chemicals, pharmaceuticals, industrial products, among other desirable products. The corresponding carboxylic acids are useful as catalysts, intermediates to acid halides, among other products.

Background Of The Invention

Gotoh et al., U.S. Patent No. 5,041,647, discloses oxidizing 1.1-dichloro-2,2,2-trifluoroethane (HCFC-123) with oxygen in the presence of water to trifluoroacetyl chloride (TFAC) accompanied by the free acid (TFAA).

Dittman, U.S. Patent No. 3,833,407 produces TFAC by reacting HCFC-123 with oxygen in the presence of active radiation.

Jacobson, U.S. Patent No 5,241,113 prepares TFAC by oxidizing HCFC-123 with oxygen over a carbon bed in the absence of water.

Childs, U.S. Patent No. 4,022,824 discloses preparing perfluoro carboxylic acid fluorides by a reaction sequence involving (1) a metathesis reaction between an unfluorinated carboxylic acid and a perfluoroacid fluoride, e.g. trifluoroacetyl fluoride (TFAF), normally prepared by electrofluorinating acetic acid), to obtain the unfluorinated carboxylic acid fluoride, followed by (2) electrofluorinating the acid fluoride product of the metathetical reaction to the desired perfluorocarboxylic acid fluoride.

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The disclosure of the previously identified U.S. Patents is hereby incorporated by reference

Cross-Reference to Related Patent

The instant invention is related to U.S. Patent No. 5,296,640, which issued on March 22, 1994 in the names of Jacobson and Ely, entitled "Process For Preparing Perhalocyl Chlorides" (corresponding to PCT Publication No. WO94/06742); the disclosure of which is hereby incorporated by reference.

Summary of the Invention

This invention provides an oxidative process for preparing polyfluoroacyl fluorides from one or more polyfluoroalkyl substituted chlorofluoromethanes and dichloromethanes.

One aspect of the invention provides perfluoroacyl fluorides and chloroperfluoroacyl fluorides from at least one perfluoroalkyl- and chloroperfluoroalkyl- substituted chlorofluoromethanes.

Another aspect of the invention relates to preparing trifluoroacetyl fluoride from a starting material comprising 1-chloro-1, 2,2,2-tetrafluoroethane.

A further aspect of the invention relates to preparing difluoroacetyl fluoride, among other difluoroacetyl derivatives, from a starting material comprising 1,1-dichloro-2,2-difluoroethane.

The invention comprises a process for preparing polyfluoroacyl fluorides having the formula X(CF₂)n COF. The process comprises contacting at least one polyfluoroalkyl dihalomethane having the formula X(CF₂)n CHClY with a source of oxygen, typically in the substantial absence of water, under conditions effective to produce said acyl fluorides, wherein X is H, Cl or F, n is 1 to 4, usually 1, and Y is Cl or F, with the proviso that when Y is Cl, X is H.

Normally, the temperature and pressure are such that the starting material(s) are at or above the critical point, e.g., the supercritical region.

In some cases X is F and n=1, and the acylfluoride comprises trifluoroacetyl fluoride, CF₃COF (TFAF), which may be accompanied by at least one of trifluoroacetyl chloride CF₃COCl (TFAC), and trifluoroacetic acid, CF₃COOH (TFAA). Normally, TFAF is the predominate product at a selectivity of at least about 50%. For example, this aspect of the invention can produce a product stream comprising at least about 60-70 mole % TFAF, about 5 to 15 mole % TFAC, about 10 to 20 mole % TFAA, about 5 to 10 mole % (CF₃CFClCFClCF₃), and about 1 to 5 mole % ClC(0)F.

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In some cases X is H and n=1 so that the acyl fluoride produced comprises diflu roacetyl fluoride, CF₂HCOF (DFAF), which may also be accompanied by at least one of difluoroacetyl chloride (DFAC), difluoroacetic acid, CHF₂COOH (DFAA), and HCF₂CCl₃. Normally, DFAF, DFAC and DFAA when taken together are produced at selectivities corresponding to at least about 50%. For example, this aspect of the invention can produce a product stream comprising about 40 to 70 mole % of at least one perhaloacetyl selected from the group of DFAC, DFAF and DFAA, about 10 to 15 mole % CF₂HCCl₃, about 4 to 10 mole % phosgene, and the remainder, if any, comprises at least one member from the group of HF, CO₂ and water.

By "supercritical region", it is meant that combination of temperature and pressure at which the density and other physical properties of the liquid and vapor phases become identical.

The inventive process is normally practiced in the substantial absence of water. By the term "in the substantial absence of water", it is meant that the amount of water present in the conversion or reaction medium as well as the starting materials is limited to that present in the starting materials, and water that may be produced in situ as a byproduct of the overall oxidation; especially when considering that the organic reactants contain chemically-bound hydrogen. Typically, the medium will contain less than about 100 ppm water. The substantial absence of water can permit the inventive process to be practiced in a manner that minimizes hydrolysis of the starting materials and/or products. It will, however, be appreciated by those skilled in this art that TFAF, TFAC, DFAF, DFAC, among other products that are obtained by the present process, may be further hydrolyzed with water to produce TFAA and DFAA.

The instant invention is an improvement in this art in that it avoids the need for a source of active radiation and eliminates the need for water or a catalyst, e.g., conventional processes employed water as a catalyst. Without wishing to be bound by any theory or explanation, it is believed that the presence of water can hydrolyze the instant products to their corresponding acids; such acids typically are not as useful for acylating agents when perhaloacylating amines and alcohols, e.g., to form amides and esters. This invention also provides a method for producing at least one of TFAF, DFAF, and related products in which the product can be separated readily from side products and unreacted starting materials, in a highly pure form, e.g., about 96 to about 99 wt % pure. This method also exhibits increased selectivity and conversion to TFAF without the concomitant formation of substantial amounts of TFAA.

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Detailed Description

The inventive process broadly comprises contacting at least one starting material as defined herein with oxygen at temperatures and pressures and for times effective to produce the desired acyl product(s). An example of the inventive process is exemplified in the following reaction relating to preparing trifluoroacetyl fluoride (equation 1):

(1) $CF_3CHClF+1/2O2 \longrightarrow CF_3COF + HCl$

Without wishing to be bound by any theory or explanation, it is believed that the presence of CF₃COCl in the product may be accounted for by competitive side reactions (equations 2 and/or 3 below):

- (2) CF₃CHClF + 1/2 O2 ----> CF₃COCl + HF
- (3) CF₃COF + HCl ----> CF₃COCl + HF

It is also believed that the reactions leading to DFAF from CHF₂CHCl₂ may be the result of the following in situ occurrences:

- (a) Oxidation of HCFC-132a to DFAC, viz. CHF₂CHCl₂ + 1/2 O2 ----> CHF₂COCl + HCl;
- (b) Oxidation decomposition of CHF₂CHCl₂ or CHF₂COCl to produce HF and H₂O; and
- (c) reaction of DFAC with HF to form DFAF, viz. CHF₂COCl + HF ----> CHF₂COF + HCl.

The aforementioned DFAF reactions may occur in any expedient sequence. It is further believed that the appearance of DFAA in the product mixture may be explained by in situ hydrolysis of DFAC or DFAF by the H₂O oxidation side product, e.g.,

 $CHF_2COX + H_2O \longrightarrow CH_2FCOOH + HX$, where x = CI or F.

Examples of other polyfluoroalkyl dihalomethane starting materials (and isomers thereof) and the polyfluoroacyl products that may be prepared therefrom in accordance with the inventive method are tabulated below:

olyacyl Products
CIF2COY, Y=F, Cl, OH
HF2CF2CF2COY, Y=F, CI, OH
CIF2CF2COY, Y=F, CI, OH
HF2COY, Y=F, Cl, OH
F3CF2COY, Y=F, CI, OH

The most significant process parameters for carrying out the reaction are temperature, pressure, and time. Normally, the higher the temperature or pressure, the shorter the time required to achieve an acceptable conversion. The

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reaction may be carried ut in a temperature range of ab ut 190 to about 320°C, and at pressures from about 400 t about 2,500 psig. Typically, temperatures of about 190° to 300°C and pressures f about 800 to 2,000 psig are employed. At temperatures and pressures below the aforementioned range, the conversion rate is relatively slow. At temperatures greater than those previously identified, the reaction conditions must be controlled to avoid side reactions which can lower the selectivity to TFAC. Pressures above the previously identified range may be employed; but the equipment costs would be higher. If desired, the reaction can be performed at relatively high temperatures by employing much shortened reaction times. Exemplification of suitable reaction times is provided hereinafter. While the specific reaction time for making a desired product will vary subject to the reaction variables identified herein, typically the reaction time will be about 10 to about 90 minutes.

While any suitable ratio of oxygen can be employed, normally the mole ratio of oxygen to the material to be oxidized can ranges from about 0.1 to about 1, with a ratio of 0.2 to 0.8 being desirable. Oxygen to oxidizable material ratios above about 1 tend to fall within the explosive range and would not be preferred. Oxygen to oxidizable material ratios below about 0.5 may reduce the desired product formation rate such that it becomes desirable to recycle unreacted starting material. The oxygen is normally diluted with one or more gases, which are inert to the oxidation environment, such as nitrogen, argon, among others, so as to keep the reaction mixture out of the explosive range and to avoid exotherms which could decompose the polyfluoroacylfluoride product(s). While any suitable oxygen source can be employed, molecular oxygen, dried air or mixtures thereof with an inert gas can be used to practice the invention.

A reactor resistant to corrosion by reaction by-products such as hydrogen fluoride, as well as chlorine and water which can come from the reaction of byproduct hydrogen chloride and oxygen, is required.

Materials useful for the reactor surfaces include silver, nickel, tantalum, nickel based alloys sold under the trademarks HASTELLOY® INCONEL® among others. Stainless steel such as 316 is typically unsatisfactory as it causes many byproducts to be produced, and its use results in decreased selectivity and conversions. Glass can be severely etched and, therefore, is not practical. ALLOY C276 sold under the trademark HASTELLOY® 276 and ALLOY 600 sold under the trademark INCONEL® are the preferred reactor materials since they exhibit minimal corrosion, and selectivity of the desired product is consistently high.

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The acyl fluoride products are isolated by any suitable standard procedure such as distillation. When the product boils below room temperature, the distillation may be carried out under pressure. For example, the purification of TFAF may be achieved by distillation under pressure using a 20 plate Oldershaw column or equivalent. Typically, TFAF is recovered by using a distillation temperature of less than about - 60°C whereas TFAC is recovered by using a distillation temperature of less than about -20°C.

The inventive oxidation process may be carried out either in a batch or continuous fashion. In either case, the process is performed in a manner sufficient to cause the oxygen and raw material to contact and form the desired product. For example, when practicing a continuous process, oxygen and at least one raw material are introduced, for example, simultaneously into a reactor. When practicing a batch process, oxygen is introduced into a reactor containing at least one raw material. In each case conditions, which are not in the explosive range for the mixture of oxygen and the material to be oxidized, are preferred.

Depending upon the desired product, the stream exiting the reactor can be recovered as a useful product, separated into its components, at least a portion recycled to the reactor, among other processing steps. An increase in the relative amount of an inert component in the starting material will in turn increase the amount of unconverted material that exits the reactor.

While the above description places particular emphasis upon oxidizing certain starting materials, the inventive process can be practiced by using any suitable raw material. Normally, the raw material will be commercially available and about 90 to about 98 % by wt. pure.

The following Examples serve to illustrate the invention, but are not intended to limit the scope of the invention.

All analyses reported in the following Examples were obtained by employing conventional gas chromatography (GC) techniques on a Hewlett-Packard Series II 5890 instrument. A 105 mx0.32 mm RTX-I (Restek Corp., Bellefonte, Pa.) capillary column was used with a thermal conductivity detector for measuring the products and byproducts. A temperature program of 40°C (15 minute hold), heating 16°C/min to 200°C (10 minute hold), and heating 50°C/min to 250°C (10 minute hold) was employed during the Examples.

"Conversion" and "selectivity" which are used herein are defined as follows. Conversion is the molar % of starting material which was consumed during the inventive oxidation process. Selectivity is defined as:

moles product or byproduct x 100% moles starting material consumed

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Example 1- TFAF

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A 400cc Hastelloy® C-276 bomb was charged with approximately 68.2g (0.5 mole) HCFC-124, and perfluoroctane as an internal standard for GC analyses. The bomb was closed and its contents were heated to about 230°C and about 600 psi pressure. Four about 200 psi injections of air from an auxiliary bomb were added at 5 minute intervals. After the final injection, the bomb was heated to a temperature of about 230°C for an additional 15 minutes to give a final pressure of about 1900 psi. The bomb was cooled to approximately -85°C before the air and HCl were vented to a caustic scrubber. The liquid contents were analyzed by gas chromatography using a high pressure syringe for sampling. The analyses indicated about 38% HCFC-124 conversion (95% conversion based on air) to a selectivity of 66% TFAF, 6% TFAC, 16% TFAA, 1% ClC(O)F and 7% (CF3CFClCFClCF3).

Example 2 - Difluoroacetyls

A 400cc Hastelloy® C-276 bomb was charged with approximately 134.9g (1.0 mole) of HCFC-132a (CF₂HCHCl₂), and carbon tetrachloride as an internal standard for gas chromatography analyses. The bomb was closed and its contents were heated to about 200°C and 450 psi pressure.

Four 100 psi injections of oxygen from an auxiliary bomb were injected at 15 minute intervals to give an approximate one hour reaction time. The bomb was cooled to about -85°C by using dry ice before HCl and any remaining oxygen were vented to a caustic scrubber. The liquid contents remaining in the bomb were analyzed by gas chromatography and showed a 46% HCFC-132a conversion to a selectivity of 15% DFAC, 15% DFAF, 24% DFAA, 13%

30 CF₂HCCl₃, and 6% phosgene. If desired, the product mixture comprising DFAF, DFAC, and DFAA can be hydrolyzed to DFAA by using known technology.

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THE FOLLOWING IS CLAIMED:

- 1. A process for preparing polyfluoroacyl fluorides having the formula X(CF₂)nCOF comprising contacting at least one polyfluoroalkyldihalomethane having the formula X(CF₂)nCHClY with an oxygen source to form a mixture, wherein said mixture is exposed to conditions sufficient to obtain said acyl fluorides, wherein X is H, Cl or F, n is 1 to 4, and Y is Cl or F, with the proviso that when Y is Cl X is H.
- 2. The process of Claim 1 wherein X is F, n is 1 and the acyl product comprises trifluoroacetyl fluoride.
 - 3. The process of Claim 1 wherein X is H and n is 1 and the product comprises difluoroacetyl fluoride, HCF₂COF.
 - 4. A product made by the process of Claim 1 comprising DFAF, DFAC and DFAA.
 - 5. A mixture comprising difluoroacetyl chloride, difluoroacetyl fluoride and difluoroacetic acid.
 - 6. A non-catalytic process for preparing at least one polyfluoroacyl halide having the formula X(CF₂)nCOF comprising contacting at least one polyfluoroalkyldihalomethane having the formula X(CF₂)nCHClY with an oxygen source to form a mixture, wherein said mixture is exposed to conditions sufficient to obtain said halide.
 - 7. The process of Claim 1 or 6 wherein said polyfluoroalkyldihalomethane comprises at least one member from the group consisting of CCIF₂CHCIF (HCFC-123a), CHF₂CF₂CF₂CHCIF (HCFC-235CA), CCIF₂CF₂CHCIF (HCFC-225CB), CHF₂CHCIF (HCFC-133), and CF₃CF₂CHCIF (HCFC-226CA)
 - 8. The process of Claim 6 wherein said halide comprises at least one member from the group consisting of CClF₂COY, Y=F, Cl, OH; CHF₂CF₂COY, Y=F, Cl, OH; CClF₂CF₂COY, Y=F, Cl, OH; CHF₂COY, Y=F, Cl, OH; and CF₃CF₂COY, Y=F, Cl, OH

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INTERNATIONAL SEARCH REPORT

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C. DOCUM	MENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the	relevant passages	Relevant to claim No.
Y	US.A.5 296 640 (JACOBSON ET AL.) 1994	22 March	1 .
	cited in the application see claim 1		
Y	EP,A,O 638 539 (SOLVAY FLUOR UND GMBH) 15 February 1995 see claim 1	DERIVATE	1
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Furt	her documents are listed to the continuation of box C.	Patent family members are fused	in annex.
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This int	ternational search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasona:	1. 1. 1
ı. 🗌	Claims Nos.: because they relate to subject matter not required to be searched by this Authority, namely:	•
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	because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically: Lack of technical measures	
	(Claims searched incompletely: 1)	
3.	Claims Nos.: because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).	
Box II	Observations where unity of invention is lacking (Continuation of item 2 of first sheet)	
	nernational Searching Authority found multiple inventions in this international application, as follows:	
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2. [As all searchable claims could be searches without effort justifying an additional fee, this Authority did not invite payment of any additional fee.	
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4.	No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:	
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	The additional search fees were accompanied by the applicant's protest.	
Romari	the additional search fees were accompanied by the applicant a protest. No protest accompanied the payment of additional search fees.	

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US	-A-5296640	22-03-94	EP-A- WO-A-	9669816 9496742	05-07-95 31-03-94
EP	-A-638539	15-02-95	DE-A- JP-A-	4342601 7053446	16-02-95 28-02-95

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